



Moorings Technical Analysis
Client: Kaly
Site: Seaweed Farm

Doc. No.: GFME-TR-090
Date: 31/05/2024

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Revision Control

| | |
|-----------|-------------|
| Doc. no.: | GFME-TR-090 |
| | |

| Rev. | Date | Originator | Approver | Description |
|------|------------|----------------|----------|-------------|
| A | 03/05/2024 | Scott Dickison | A.Young | First Issue |
| | | | | |
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1 Summary

This report describes a Technical Analysis for a seaweed farm arrangement for Kaly.

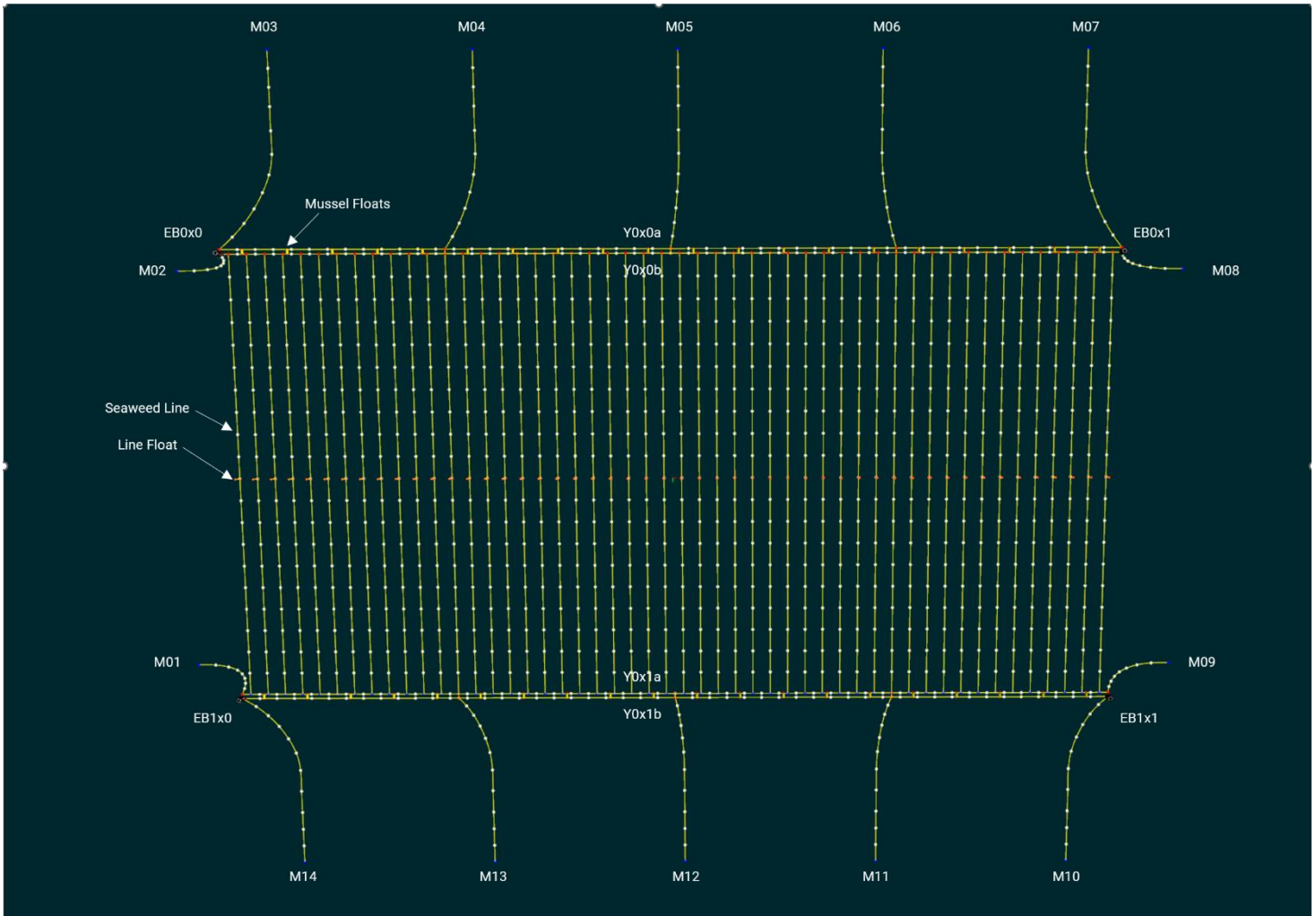
The report describes the applied environmental data, the processing undertaken to enable that data to be used for the analysis, the physical design being analysed, the results of that analysis and the compliance of the design to the design standard requested.

For the purposes of developing a standard system, a set of environments will be applied in all directions. Environment 1 is based on the 50 year current in Loch Snizort, with a typical wind speed and sheltered wave. This environmental case has been processed using the guidelines in Scottish Technical Standard for Finfish Aquaculture. An additional 2 environments have been modelled to indicate the performance of the grid across a range of sheltered conditions.

The tables below show the highest loaded lines in the harvest state of environment 1 and their factors of safety compared with the requirement of the standard for a given material.

| Line | Segment | Max Tension ULS (T) | Min FOS ULS | Found in | ULS Material Factor |
|---------------|-----------------------|---------------------|-------------|----------|---------------------|
| Mooring02 | PolySteel_3_Strand_32 | 11.44 | 1.42 | ULS01 | 3.00 |
| | U2_StudLink_32 | 11.44 | 5.19 | ULS01 | 2.00 |
| GridlineY0x0a | PolySteel_3_Strand_32 | 4.17 | 3.90 | ULS01 | 3.00 |
| GridlineY0x0b | PolySteel_3_Strand_32 | 6.75 | 2.41 | ULS01 | 3.00 |

It is recommended that embedment tests should be carried out at all intended anchor locations to ensure the expected holding power of the anchor can be achieved.



2 Introduction

Gael Force Group has been instructed to carry out a Technical Analysis for Kaly for a seaweed farm design. The Site consists of 4 rectangular grids, independently moored, with space allowance for creel fishing corridors.

This document outlines the inputs and results from a full technical dynamic analysis for the above system design. It will describe the physical system parameters and environmental conditions used as the basis for the design, and adjustments required by the applied design standard. All system loads are identified and evaluated.

3 Design Basis

3.1 Assumptions

The following assumptions have been made in preparing and undertaking this analysis –

1. Seabed depth of 20m
2. A seaweed model has been determined based on physical data from SINTEF research organisation.
3. No effects of current shadowing have been considered.
4. The requirement of each component will be the same for those in symmetrical positions

3.2 Applicable Design Standard

The system has been analysed applying the requirements of Scottish Technical Standard for Finfish Aquaculture. This is for environmental processing only and as a reference for possible equipment assignment. Forty-two simulations have been undertaken which are referred to as Ultimate Limit State (ULS) simulations. These consist of the applied environment in eight directions for the first environmental case and 3 for each additional environment to cover 3 unique directions for this symmetrical arrangement as well as three growth states for the seaweed. These are starting mass, mid growth and harvest growth.

The results of these simulations are post-processed to identify the highest load scenario for every component within the system.

The loads on every component are then compared to the Minimum Break Load specified for that component to confirm it complies with all the minimum factors of safety specified within the Standard.

It has been assumed that all anchors are fully embedded and are therefore considered as being fixed points.

3.3 Environmental Conditions

Table 1: Maximum combined waves (wind waves & ocean waves)

| Environment: | 1 | 2 | 3 |
|----------------------------------|-------|-------|-------|
| U (m ^{s⁻¹}) | 34.34 | 30.00 | 20.00 |
| H _s (m) | 1.05 | 0.79 | 0.53 |
| T _P (s) | 5.00 | 4.00 | 3.00 |

Table 2: Current

| Environment: | 1 | 2 | 3 |
|---|-------|-----|-----|
| V _c (m ^{s⁻¹}) | 0.274 | 0.2 | 0.1 |

3.4 Mooring System

The system as designed for installation at site is identified in the tables below –

Table 3: Mooring Line Details

| Mooring Line | Depth[m] | Segment | Segment Length (m) | Anchor Weight [T] |
|--------------|----------|-----------------------|--------------------|-------------------|
| Mooring01 | | PolySteel_3_Strand_32 | 46.25 | Helical |
| Mooring01 | | U2_StudLink_32 | 13.75 | |
| Mooring02 | | PolySteel_3_Strand_32 | 46.25 | Helical |
| Mooring02 | | U2_StudLink_32 | 13.75 | |
| Mooring03 | | PolySteel_3_Strand_32 | 46.25 | 0.5 |
| Mooring03 | | U2_StudLink_32 | 13.75 | |
| Mooring04 | | PolySteel_3_Strand_32 | 46.25 | 0.5 |
| Mooring04 | | U2_StudLink_32 | 13.75 | |
| Mooring05 | | PolySteel_3_Strand_32 | 46.25 | 0.5 |
| Mooring05 | | U2_StudLink_32 | 13.75 | |
| Mooring06 | | PolySteel_3_Strand_32 | 46.25 | 0.5 |
| Mooring06 | | U2_StudLink_32 | 13.75 | |
| Mooring07 | | PolySteel_3_Strand_32 | 46.25 | 0.5 |
| Mooring07 | | U2_StudLink_32 | 13.75 | |
| Mooring08 | | PolySteel_3_Strand_32 | 20.25 | Helical |
| Mooring08 | | U2_StudLink_32 | 13.75 | |
| Mooring09 | | PolySteel_3_Strand_32 | 20.25 | Helical |
| Mooring09 | | U2_StudLink_32 | 13.75 | |
| Mooring10 | | PolySteel_3_Strand_32 | 20.25 | 0.5 |
| Mooring10 | | U2_StudLink_32 | 13.75 | |
| Mooring11 | | PolySteel_3_Strand_32 | 20.25 | 0.5 |
| Mooring11 | | U2_StudLink_32 | 13.75 | |
| Mooring12 | | PolySteel_3_Strand_32 | 20.25 | 0.5 |
| Mooring12 | | U2_StudLink_32 | 13.75 | |
| Mooring13 | | PolySteel_3_Strand_32 | 20.25 | 0.5 |
| Mooring13 | | U2_StudLink_32 | 13.75 | |
| Mooring14 | | PolySteel_3_Strand_32 | 20.25 | 0.5 |
| Mooring14 | | U2_StudLink_32 | 13.75 | |

Table 4: Grid Line Details

| Grid Line | Segment | Length |
|-------------------------|-----------------------|--------|
| Longitudinal Grid Lines | PolySteel_3_Strand_32 | 200 |
| Transverse Grid Lines | Seaweed Line | 100 |

Table 5: Buoy Details

| Buoy No. | Buoy Type | Size (l) |
|---------------|--------------|----------|
| EB0x0 | End Buoy | 600 |
| EB0x1 | End Buoy | 600 |
| EB1x0 | End Buoy | 600 |
| EB1x1 | End Buoy | 600 |
| Mussel Floats | Mussel Float | 200 |
| Line Floats | Polyform | A0 |

3.5 Modelling

3.5.1 Moorings Analysis Overview

Proteus DS software has been used for computer modelling and simulation of mooring installations. Other software packages are used in the industry however Proteus DS was chosen due to the extensive validation of the software undertaken by DSA, including tank tests, software benchmarks, full-scale comparison and, in conjunction with Gael Force’s own comprehensive empirical real-time data sets was considered the most suitable dynamic simulation software for the purpose.

The Finite Element Analysis process does not design a mooring system, it enables the User to analyse a specified design to confirm the loads exerted upon it and the stresses in the components. As such the physical design of the system along with the characteristics of the mooring system components are modelled in the software. The environmental conditions are applied to the model based on the wind, waves and currents, and the stresses within the components are calculated.

As modelled, we have analysed 1 grid of the seaweed farm arrangement. The grid is independently moored. It consists of a pair of headlines (double gridlines) each with 20 headline mussel floats, equally spaced. The headlines are terminated by a 600L buoy at each end. Mooring lines are attached to the headline at the ends and at 50m spacing along the side. The end mooring lines are terminated by helical anchors with a scope of 1.5 while the side mooring lines are terminated by drag anchors with a scope of 3. These headlines support 50 seaweed lines with 4m spacing. Each seaweed line features a midline buoy with a 1.5m connector.

A model for seaweed drag has been created using physical test data found in OMAE2019-96375 CURRENT INDUCED DRAG FORCES ON CULTIVATED SUGAR KELP⁽²⁾. This document features the chart in Figure 1 - Drag force per meter divided by weight per meter (n) as a function of towing velocity

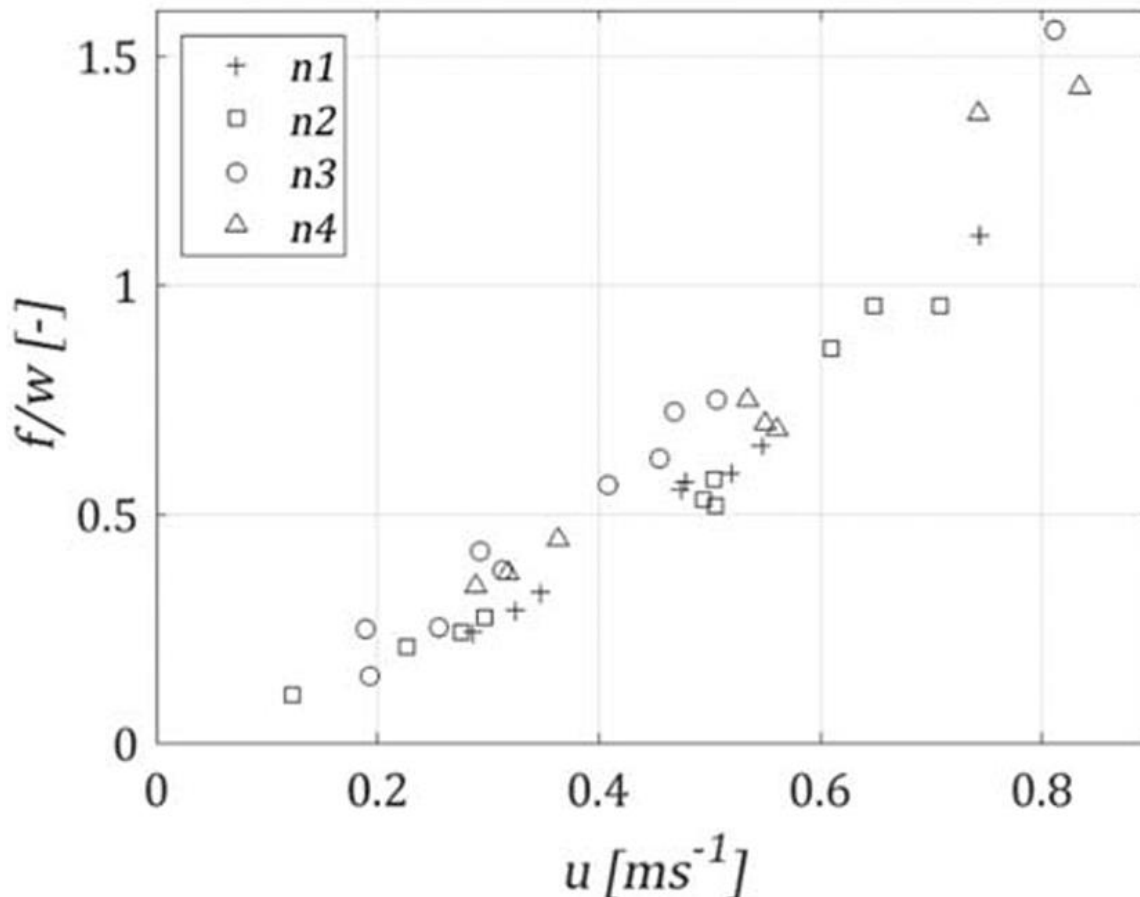


Figure 1 - Drag force per meter divided by weight per meter (n) as a function of towing velocity

The seaweed line is modelled in proteus as a flexible cylinder with a density of 1024kg/m³. Diameter is used to set the appropriate mass per meter. This Diameter is used as the wetted area in the drag calculation using the formula:

$$C_d = \frac{2 * F_d}{\rho u^2 * A}$$

Drag is calculated for each mass/m of seaweed at various velocities and a quadratic line of best fit is applied.

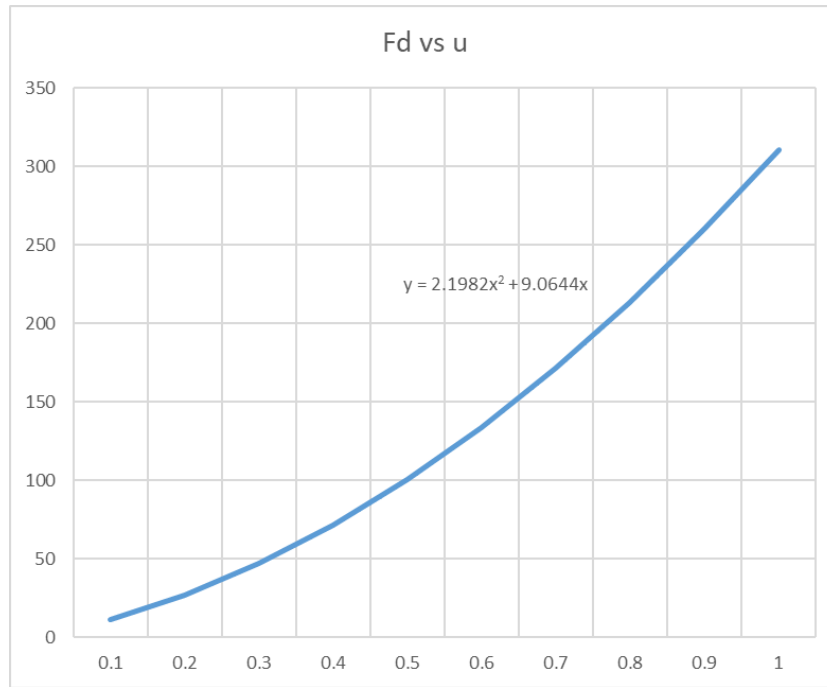


Figure 2 - Drag force as a function of velocity for seaweed at 16kg/m

Assuming zero drag at zero velocity, the equation of the line of best fit is used as input for the linear quadratic drag model in proteus for each analysed growth state. Axial and normal drag has been considered equal.

| Seaweed kg/m | LinearNormal DragCoefficient (Ns/m ²) | LinearTangential DragCoefficient (Ns/m ²) | QuadraticNormal DragCoefficient (Ns ² /m ³) | QuadraticTangential DragCoefficient (Ns ² /m ³) |
|--------------|---|---|--|--|
| 5 (start) | 28.33 | 28.33 | 68.69 | 68.69 |
| 10 (mid) | 56.65 | 56.65 | 137.39 | 137.39 |
| 16 (harvest) | 90.06 | 90.06 | 219.82 | 219.82 |

The original data source states “the results of this study may overestimate the drag force rather than underestimate (for growth levels similar to the ones presented in this study) and might therefore still be of interest for dimensioning of seaweed farms”. In addition to this, the effects of current shadowing on seaweed lines located behind other seaweed lines is difficult to predict without additional data and has not been included. Therefore, results within this report should be considered as conservative.

The model is run initially with no environmental conditions applied to it, for a simulated period of 30 seconds to allow it to settle to a state of equilibrium, the current is then added for a simulated period of 180 seconds, following which the waves are added for a duration of two times the wave period.

3.5.2 Mooring System Component Identification

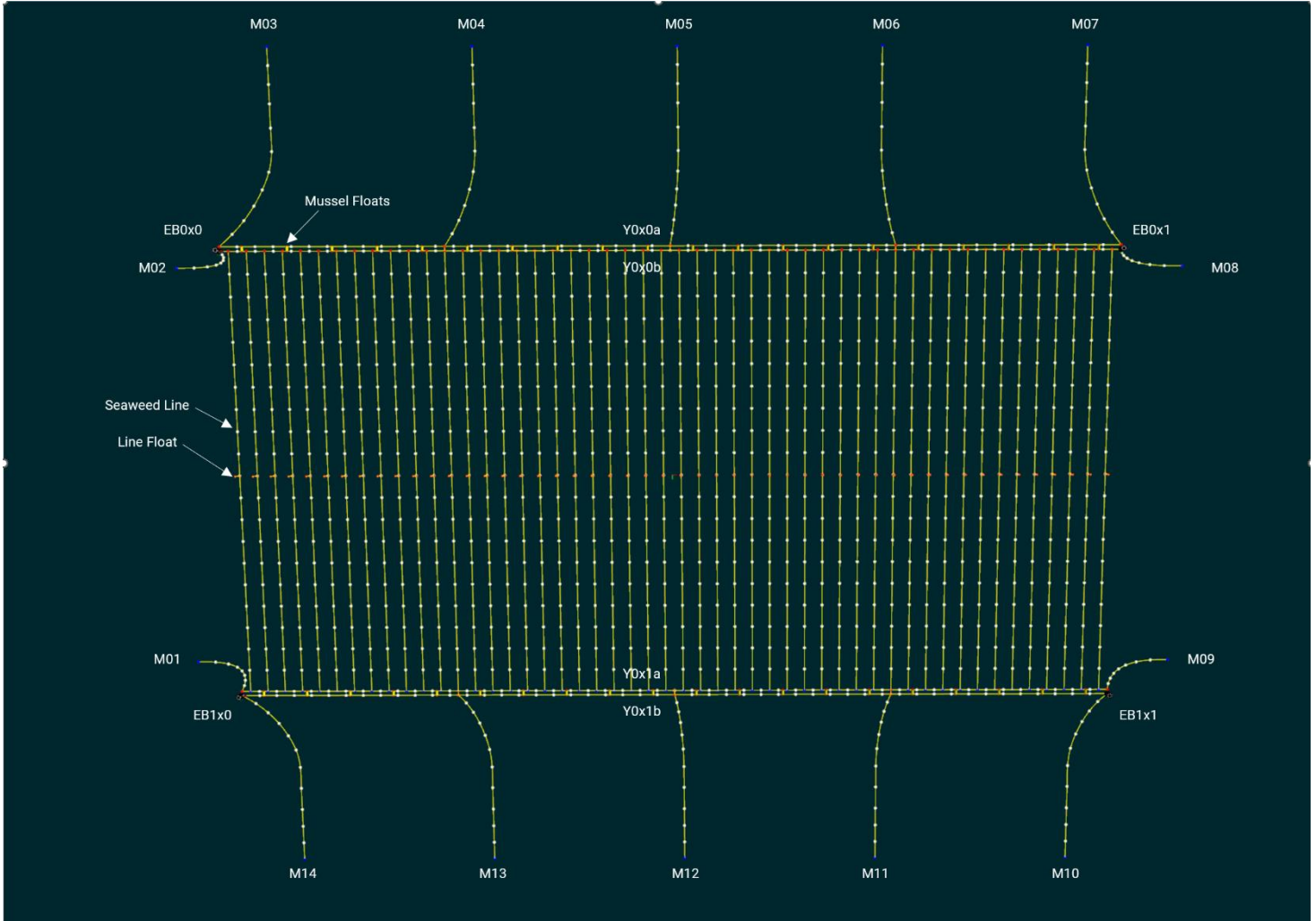


Figure 3 - Mooring System Component Identification

4 Results

4.1 Analyses Condition Inputs

The environmental conditions have been transposed to ensure all parameters follow the same convention in respect of direction.

When applied to the model the wave height is converted to H_{max} by multiplying the H_s value by 1.9. The environmental conditions used for the purpose of analysis are identified in Table 6: Environmental conditions for analyses. Simulations have been assigned into groups that will be processed together and their maximum loads compared.

Table 6: Environmental conditions for analyses

| Group | Analysis | Direction (°T) | H_{max} (m) | $T_{p(P-M)}$ (s) | Wind (ms^{-1}) | Current (ms^{-1}) |
|-------|-------------------|----------------|---------------|------------------|--------------------|-----------------------|
| 1 | ULS01_Harvest_0 | 0° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS02_Harvest_45 | 45° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS03_Harvest_90 | 90° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS04_Harvest_135 | 135° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS05_Harvest_180 | 180° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS06_Harvest_225 | 225° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS07_Harvest_270 | 270° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS08_Harvest_315 | 315° | 2.00 | 5.00 | 33.34 | 0.274 |
| 2 | ULS09_Mid_0 | 0° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS10_Mid_45 | 45° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS11_Mid_90 | 90° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS12_Mid_135 | 135° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS13_Mid_180 | 180° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS14_Mid_225 | 225° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS15_Mid_270 | 270° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS16_Mid_315 | 315° | 2.00 | 5.00 | 33.34 | 0.274 |
| 3 | ULS17_Start_0 | 0° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS18_Start_45 | 45° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS19_Start_90 | 90° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS20_Start_135 | 135° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS21_Start_180 | 180° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS22_Start_225 | 225° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS23_Start_270 | 270° | 2.00 | 5.00 | 33.34 | 0.274 |
| | ULS24_Start_315 | 315° | 2.00 | 5.00 | 33.34 | 0.274 |
| 4 | ULS25_Harvest2_0 | 0° | 1.5 | 4.00 | 30.00 | 0.2 |
| | ULS26_Harvest2_45 | 45° | 1.5 | 4.00 | 30.00 | 0.2 |
| | ULS27_Harvest2_90 | 90° | 1.5 | 4.00 | 30.00 | 0.2 |
| 5 | ULS28_Harvest3_0 | 0° | 1.0 | 3.00 | 20.00 | 0.1 |
| | ULS29_Harvest3_45 | 45° | 1.0 | 3.00 | 20.00 | 0.1 |
| | ULS30_Harvest3_90 | 90° | 1.0 | 3.00 | 20.00 | 0.1 |
| 6 | ULS31_Mid2_0 | 0° | 1.5 | 4.00 | 30.00 | 0.2 |
| | ULS32_Mid2_45 | 45° | 1.5 | 4.00 | 30.00 | 0.2 |
| | ULS33_Mid2_90 | 90° | 1.5 | 4.00 | 30.00 | 0.2 |
| 7 | ULS34_Mid3_0 | 0° | 1.0 | 3.00 | 20.00 | 0.1 |
| | ULS35_Mid3_45 | 45° | 1.0 | 3.00 | 20.00 | 0.1 |
| | ULS36_Mid3_90 | 90° | 1.0 | 3.00 | 20.00 | 0.1 |
| 8 | ULS37_Start2_0 | 0° | 1.5 | 4.00 | 30.00 | 0.2 |
| | ULS38_Start2_45 | 45° | 1.5 | 4.00 | 30.00 | 0.2 |
| | ULS39_Start2_90 | 90° | 1.5 | 4.00 | 30.00 | 0.2 |
| 9 | ULS40_Start3_0 | 0° | 1.0 | 3.00 | 20.00 | 0.1 |
| | ULS41_Start3_45 | 45° | 1.0 | 3.00 | 20.00 | 0.1 |
| | ULS42_Start3_90 | 90° | 1.0 | 3.00 | 20.00 | 0.1 |

4.2 Evaluation of Simulation Results

The dimensioning loads in the following tables, Table 7: Highest Loaded Mooring Lines , Table 8 Highest Loaded Grid Lines , are identified based on whether the highest load occurs in either an Ultimate Limit State or an Accident Limit State scenario. The component will be dimensioned according to whichever state & environment in which the highest calculated Minimum Break Load is specified. Given the environments have been applied in all directions, it can be assumed that the requirement of each component will be the same for those in symmetrical positions.

4.2.1 Component Line Loads – Harvest State across all environments

Table 7: Highest Loaded Mooring Lines in the Harvest State – Environment 1

| Mooring | Study in which Max Load Obtained | Dim Load(T) | ULS Minimum Breaking Load (MBL)(T) | |
|-----------|----------------------------------|-------------|------------------------------------|-----------------|
| | | ULS | Rope | Chain / Shackle |
| | | yl = 1.15 | ym = 3.00 | ym = 2.00 |
| Mooring01 | ULS01_Harvest_0 | 11.44 | 34.33 | 22.89 |
| Mooring02 | ULS01_Harvest_0 | 11.44 | 34.33 | 22.88 |
| Mooring03 | ULS03_Harvest_90 | 3.79 | 11.37 | 7.58 |
| Mooring04 | ULS03_Harvest_90 | 7.68 | 23.03 | 15.35 |
| Mooring05 | ULS03_Harvest_90 | 7.56 | 22.67 | 15.11 |
| Mooring06 | ULS03_Harvest_90 | 7.68 | 23.03 | 15.35 |
| Mooring07 | ULS03_Harvest_90 | 3.79 | 11.36 | 7.58 |
| Mooring08 | ULS05_Harvest_180 | 11.44 | 34.33 | 22.89 |
| Mooring09 | ULS05_Harvest_180 | 11.44 | 34.32 | 22.88 |
| Mooring10 | ULS07_Harvest_270 | 3.81 | 11.43 | 7.62 |
| Mooring11 | ULS07_Harvest_270 | 7.72 | 23.17 | 15.45 |
| Mooring12 | ULS07_Harvest_270 | 7.58 | 22.75 | 15.17 |
| Mooring13 | ULS07_Harvest_270 | 7.72 | 23.15 | 15.43 |
| Mooring14 | ULS07_Harvest_270 | 3.81 | 11.44 | 7.63 |

Table 8 Highest Loaded Grid Lines in the Harvest State – Environment 1

| Gridline | Study in which Max Load Obtained | Dim Load(T) | ULS Minimum Breaking Load (MBL)(T) | |
|---------------|----------------------------------|-------------|------------------------------------|-----------------|
| | | ULS | Rope | Chain / Shackle |
| | | yl = 1.15 | ym = 3.00 | ym = 2.00 |
| GridlineY0x0b | ULS05_Harvest_180 | 6.75 | 20.25 | 13.50 |
| GridlineY0x1b | ULS05_Harvest_180 | 4.17 | 12.50 | 8.33 |
| GridlineY0x0a | ULS05_Harvest_180 | 4.17 | 12.50 | 8.33 |
| GridlineY0x1a | ULS01_Harvest_0 | 6.75 | 20.25 | 13.50 |

Table 9: Highest Loaded Mooring Lines in the Harvest State – Environment 2

| Mooring | Study in which Max Load Obtained | Dim Load(T) | ULS Minimum Breaking Load (MBL)(T) | |
|-----------|----------------------------------|-------------|------------------------------------|---|
| | | ULS | Rope | Coupling plates / Steel coupling elements / Chain |
| | | yl = 1.15 | ym = 3.00 | ym = 2.00 |
| Mooring01 | ULS25_Harvest2_0 | 7.44 | 22.33 | 14.89 |
| Mooring02 | ULS25_Harvest2_0 | 7.44 | 22.31 | 14.87 |
| Mooring03 | ULS27_Harvest2_90 | 2.66 | 7.97 | 5.32 |
| Mooring04 | ULS27_Harvest2_90 | 5.23 | 15.70 | 10.47 |
| Mooring05 | ULS27_Harvest2_90 | 5.14 | 15.41 | 10.27 |
| Mooring06 | ULS27_Harvest2_90 | 5.24 | 15.71 | 10.47 |
| Mooring07 | ULS27_Harvest2_90 | 2.66 | 7.98 | 5.32 |

Table 10 Highest Loaded Grid Lines in the Harvest State – Environment 2

| Gridline | Study in which Max Load Obtained | Dim Load(T) | ULS Minimum Breaking Load (MBL)(T) | |
|---------------|----------------------------------|-------------|------------------------------------|---|
| | | ULS | Rope | Coupling plates / Steel coupling elements / Chain |
| | | yl = 1.15 | ym = 3.00 | ym = 2.00 |
| GridlineY0x0b | ULS25_Harvest2_0 | 4.35 | 13.05 | 8.70 |
| GridlineY0x1b | ULS25_Harvest2_0 | 2.40 | 7.20 | 4.80 |

Table 11: Highest Loaded Mooring Lines in the Harvest State – Environment 3

| Mooring | Study in which Max Load Obtained | Dim Load(T) | ULS Minimum Breaking Load (MBL)(T) | |
|-----------|----------------------------------|-------------|------------------------------------|---|
| | | ULS | Rope | Coupling plates / Steel coupling elements / Chain |
| | | yl = 1.15 | ym = 3.00 | ym = 2.00 |
| Mooring01 | ULS28_Harvest3_0 | 2.44 | 7.33 | 4.88 |
| Mooring02 | ULS29_Harvest3_45 | 2.87 | 8.60 | 5.73 |
| Mooring03 | ULS30_Harvest3_90 | 1.26 | 3.79 | 2.53 |
| Mooring04 | ULS30_Harvest3_90 | 2.30 | 6.89 | 4.59 |
| Mooring05 | ULS30_Harvest3_90 | 2.24 | 6.71 | 4.48 |
| Mooring06 | ULS30_Harvest3_90 | 2.29 | 6.87 | 4.58 |
| Mooring07 | ULS30_Harvest3_90 | 1.26 | 3.79 | 2.53 |

Table 12 Highest Loaded Grid Lines in the Harvest State – Environment 3

| Gridline | Study in which Max Load Obtained | Dim Load(T) | ULS Minimum Breaking Load (MBL)(T) | |
|---------------|----------------------------------|-------------|------------------------------------|---|
| | | ULS | Rope | Coupling plates / Steel coupling elements / Chain |
| | | yl = 1.15 | ym = 3.00 | ym = 2.00 |
| GridlineY0x0b | ULS29_Harvest3_45 | 2.20 | 6.61 | 4.41 |
| GridlineY0x1b | ULS28_Harvest3_0 | 0.58 | 1.73 | 1.15 |

4.2.2 Loads across environmental and growth states

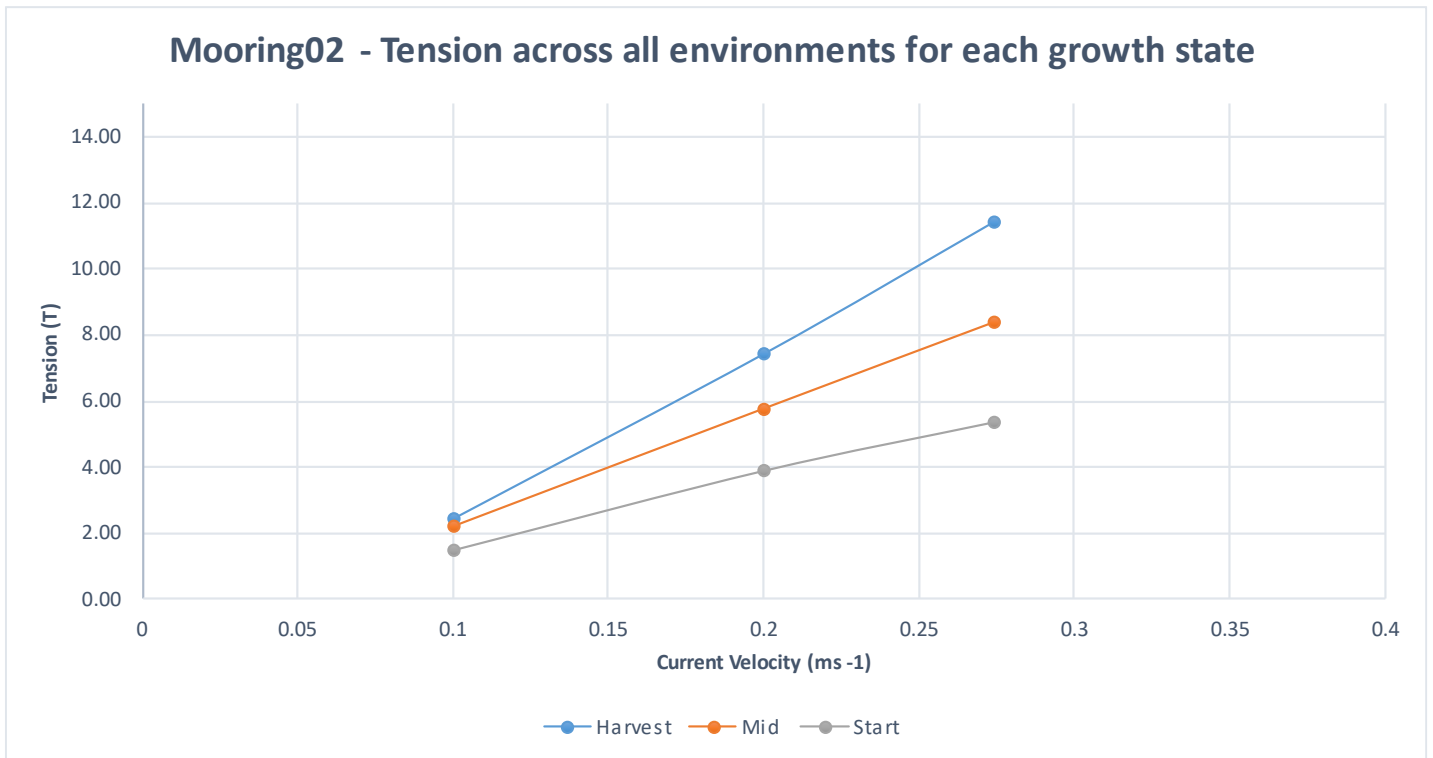


Figure 4 - Highest Loads in Mooring02 across all states

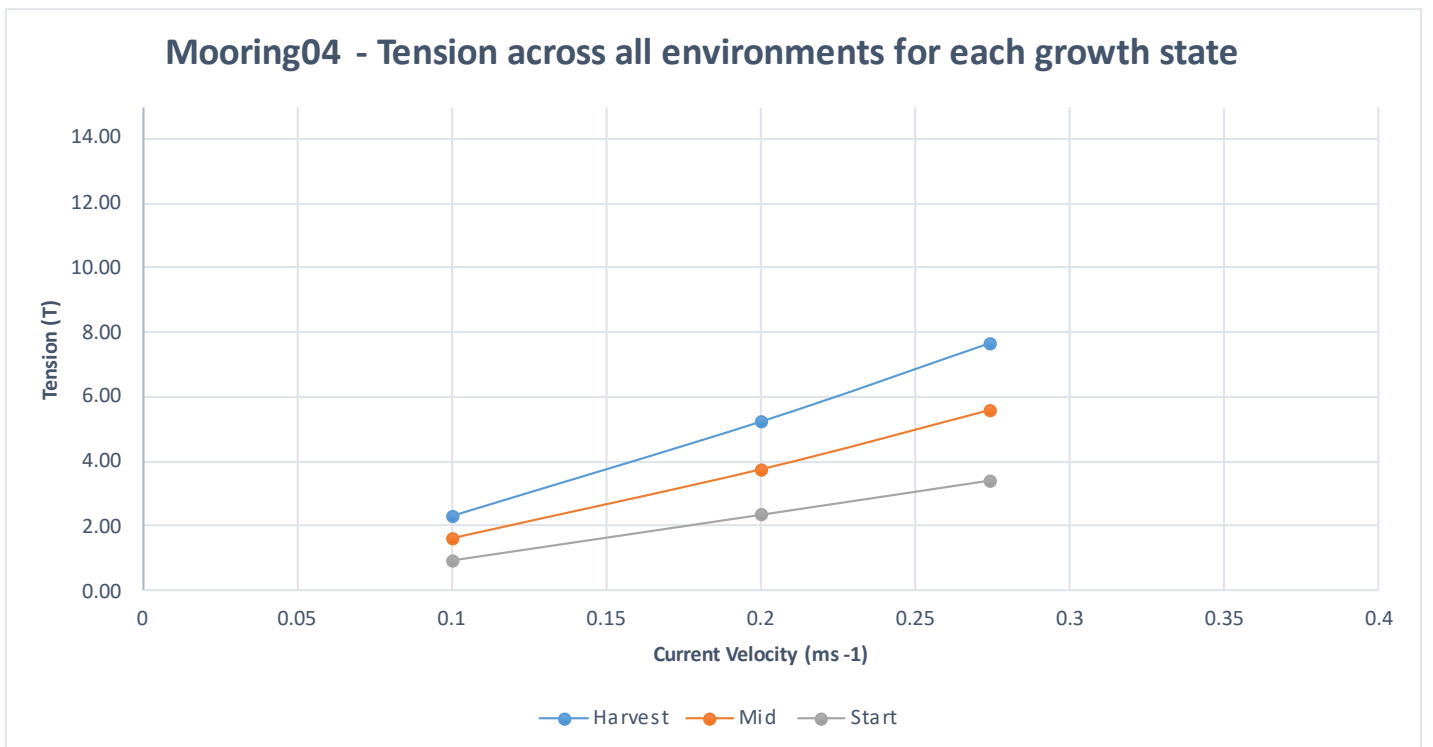


Figure 5 - Highest Loads in Mooring04 across all states

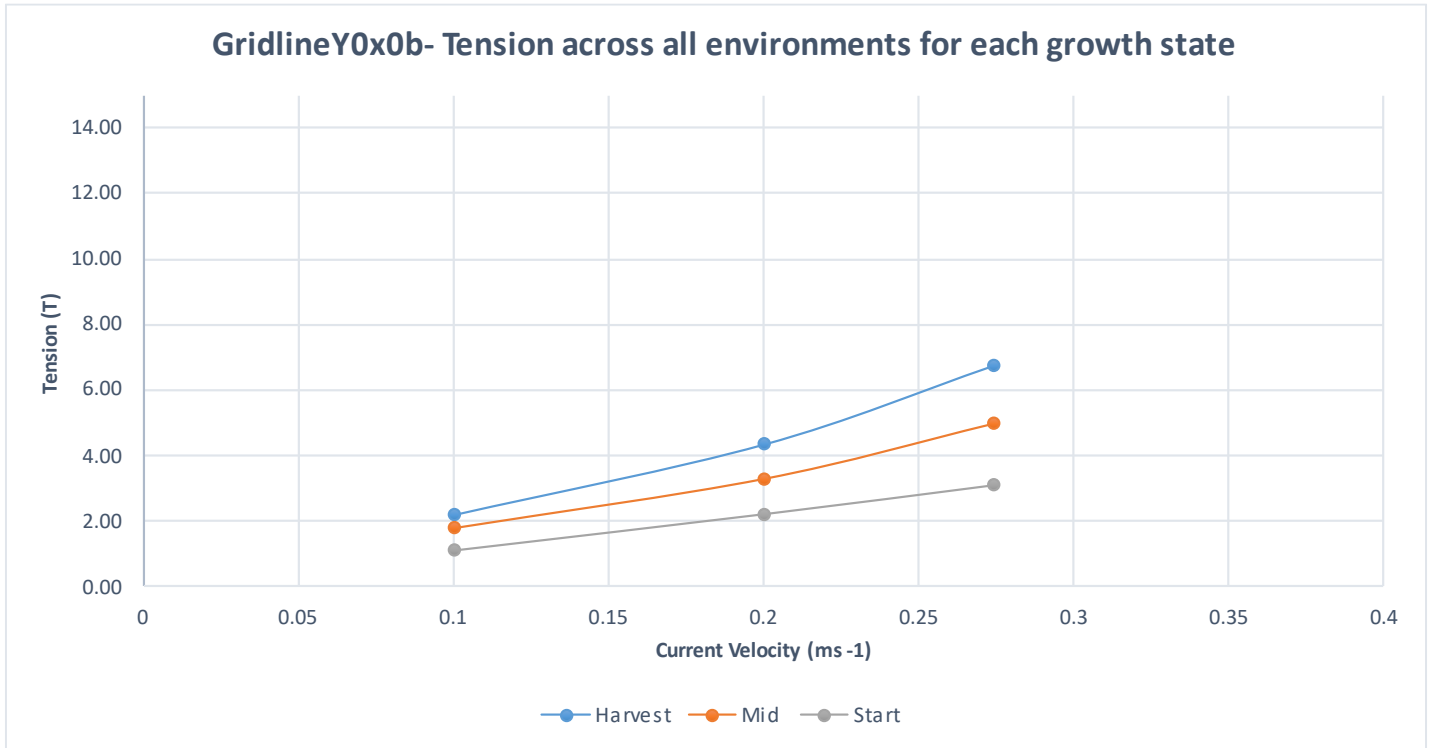


Figure 6 - Highest loads in GridlineY0x0b across all states

PROTEUS DS

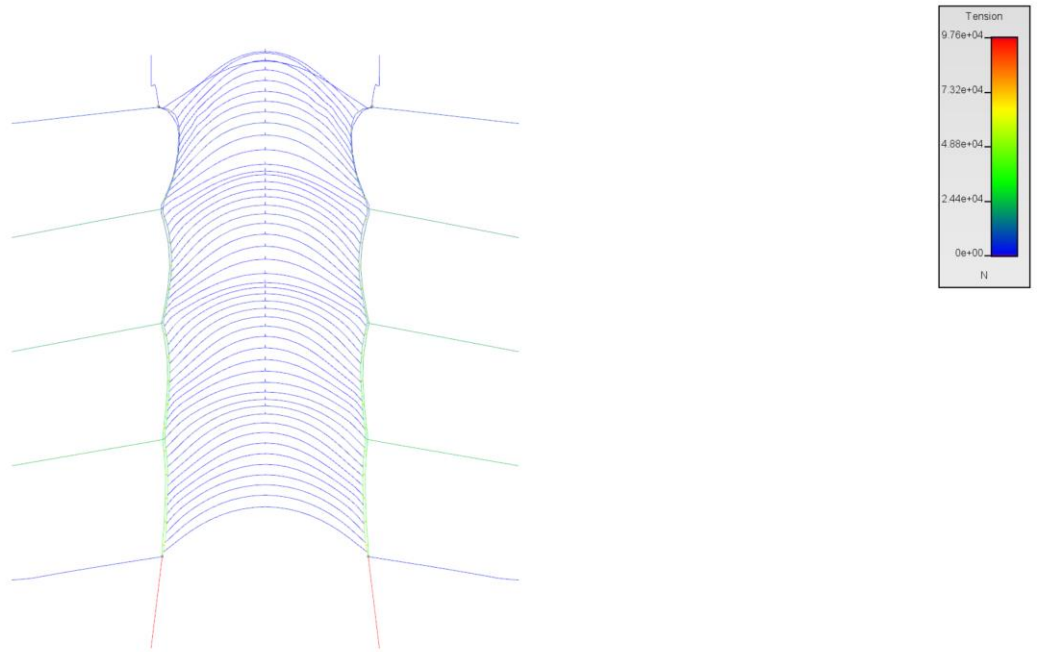


Figure 7 - ULS01 - Tension

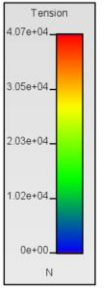
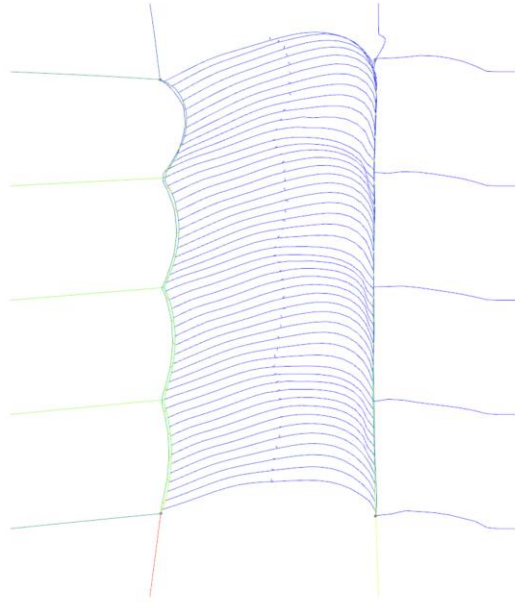


Figure 8 - ULS02 - Tension

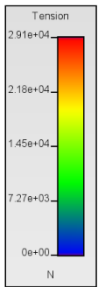
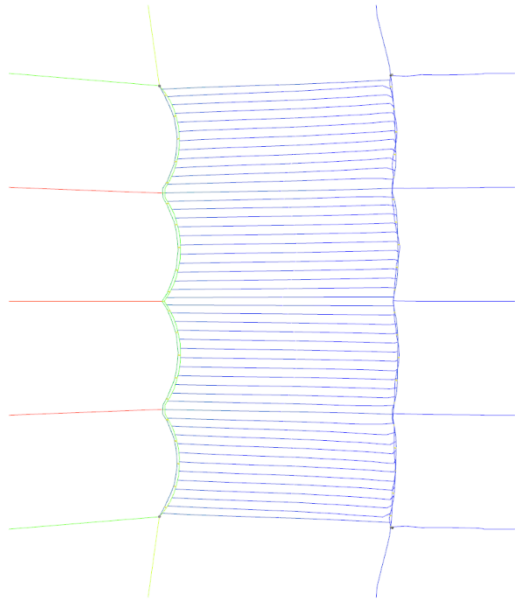


Figure 9 - ULS03 - Tension

4.2.3 Buoys – Submersion

In the simulations a virtual probe is located in all buoys enabling the buoy submersion to be recorded. Table 13: Highest Buoy Submersion identifies the maximum submersion each buoy experiences and the study in which it experiences it.

Table 13: Highest Buoy Submersion in Harvest State – Environment 1

| Buoy No. | Study With Deepest Submersion | Submersion (m) |
|----------|-------------------------------|----------------|
| EB0x0 | ULS01_Harvest_0 | -7.60 |
| EB0x1 | ULS05_Harvest_180 | -7.60 |
| EB1x0 | ULS01_Harvest_0 | -7.60 |
| EB1x1 | ULS05_Harvest_180 | -7.60 |
| MF0x01 | ULS01_Harvest_0 | -7.67 |
| MF0x02 | ULS01_Harvest_0 | -6.03 |
| MF0x03 | ULS02_Harvest_45 | -4.98 |
| MF0x04 | ULS02_Harvest_45 | -4.44 |
| MF0x05 | ULS02_Harvest_45 | -4.44 |
| MF0x06 | ULS03_Harvest_90 | -4.08 |
| MF0x07 | ULS03_Harvest_90 | -3.01 |
| MF0x08 | ULS03_Harvest_90 | -2.65 |
| MF0x09 | ULS03_Harvest_90 | -2.99 |
| MF0x10 | ULS03_Harvest_90 | -4.00 |
| MF0x11 | ULS03_Harvest_90 | -4.00 |
| MF0x12 | ULS03_Harvest_90 | -2.99 |
| MF0x13 | ULS03_Harvest_90 | -2.65 |
| MF0x14 | ULS03_Harvest_90 | -3.01 |
| MF0x15 | ULS03_Harvest_90 | -4.09 |
| MF0x16 | ULS04_Harvest_135 | -4.44 |
| MF0x17 | ULS04_Harvest_135 | -4.44 |
| MF0x18 | ULS04_Harvest_135 | -4.98 |
| MF0x19 | ULS05_Harvest_180 | -6.03 |
| MF0x20 | ULS05_Harvest_180 | -7.67 |
| MF1x01 | ULS01_Harvest_0 | -7.67 |
| MF1x02 | ULS01_Harvest_0 | -6.03 |
| MF1x03 | ULS08_Harvest_315 | -4.96 |
| MF1x04 | ULS08_Harvest_315 | -4.42 |
| MF1x05 | ULS08_Harvest_315 | -4.42 |
| MF1x06 | ULS07_Harvest_270 | -4.09 |
| MF1x07 | ULS07_Harvest_270 | -3.01 |
| MF1x08 | ULS07_Harvest_270 | -2.65 |
| MF1x09 | ULS07_Harvest_270 | -2.99 |
| MF1x10 | ULS07_Harvest_270 | -4.00 |
| MF1x11 | ULS07_Harvest_270 | -4.00 |
| MF1x12 | ULS07_Harvest_270 | -2.99 |
| MF1x13 | ULS07_Harvest_270 | -2.65 |
| MF1x14 | ULS07_Harvest_270 | -3.00 |
| MF1x15 | ULS07_Harvest_270 | -4.07 |
| MF1x16 | ULS06_Harvest_225 | -4.42 |
| MF1x17 | ULS06_Harvest_225 | -4.42 |
| MF1x18 | ULS06_Harvest_225 | -4.96 |
| MF1x19 | ULS05_Harvest_180 | -6.03 |
| MF1x20 | ULS05_Harvest_180 | -7.67 |

The values highlighted in bold are the deepest submerged buoys of each type across all studies. The plot of these buoys have been provided in the following figures.

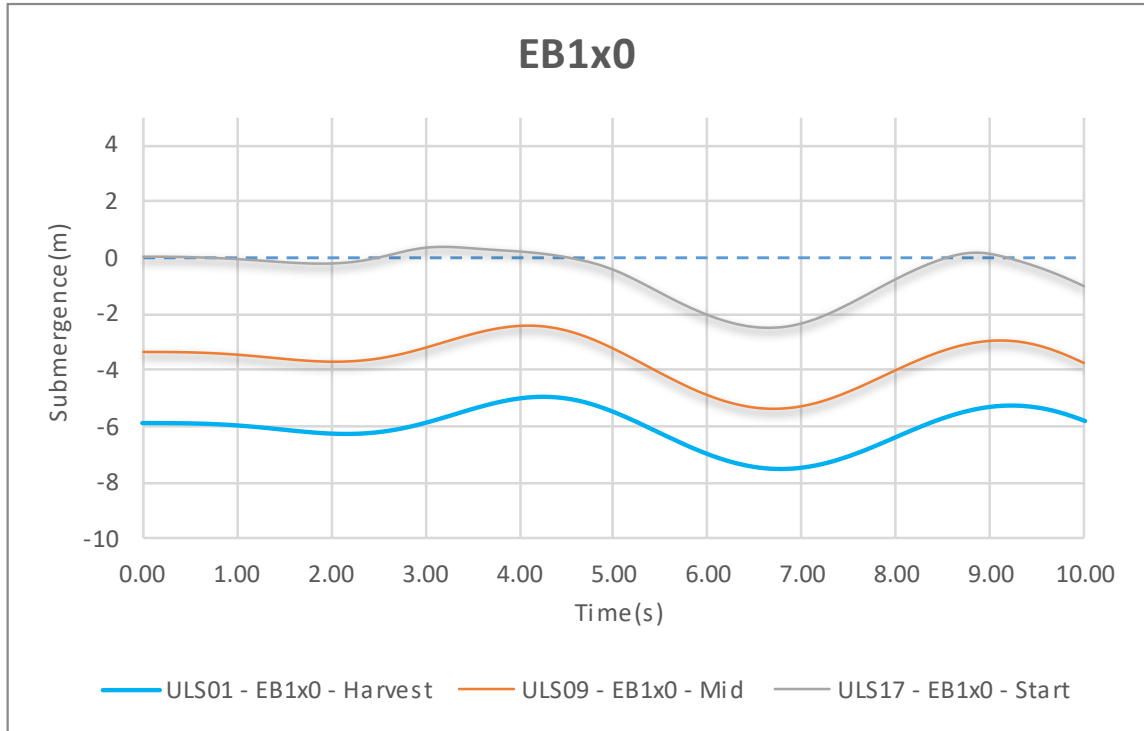


Figure 10 - Buoy Simulation – buoy EB1x0 submersion end buoy – Environment 1

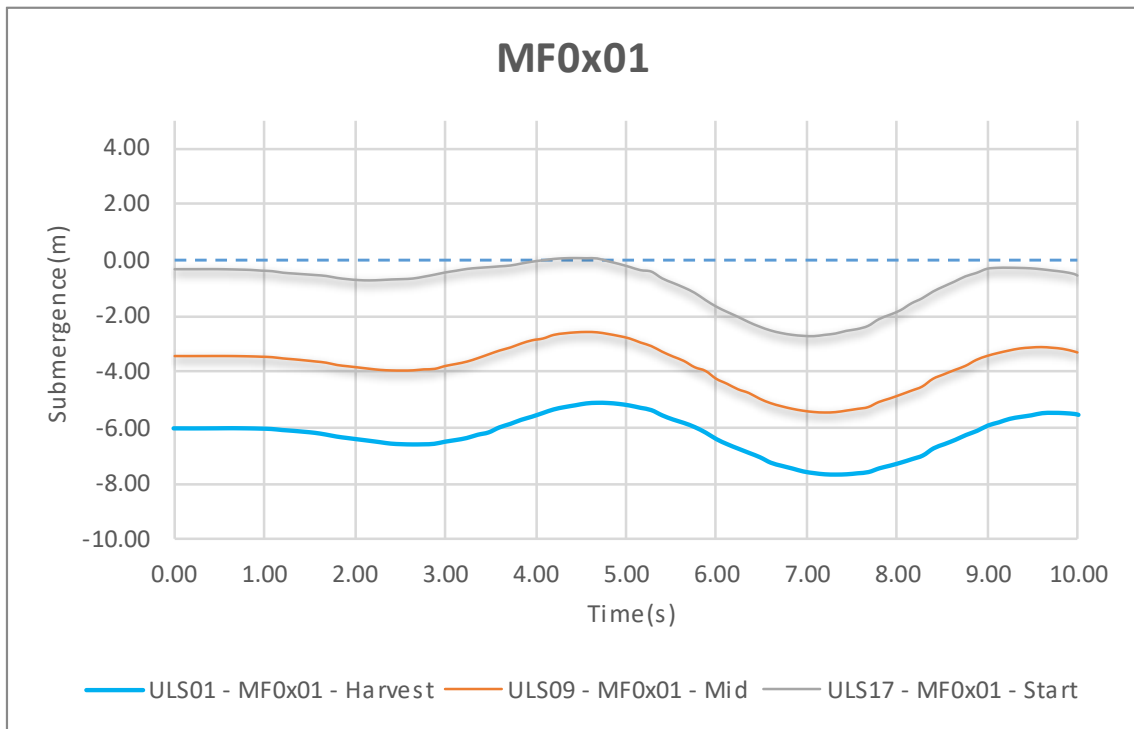


Figure 11 - Buoy Simulation – buoy MF0x01 submersion mussel floats – Environment 1

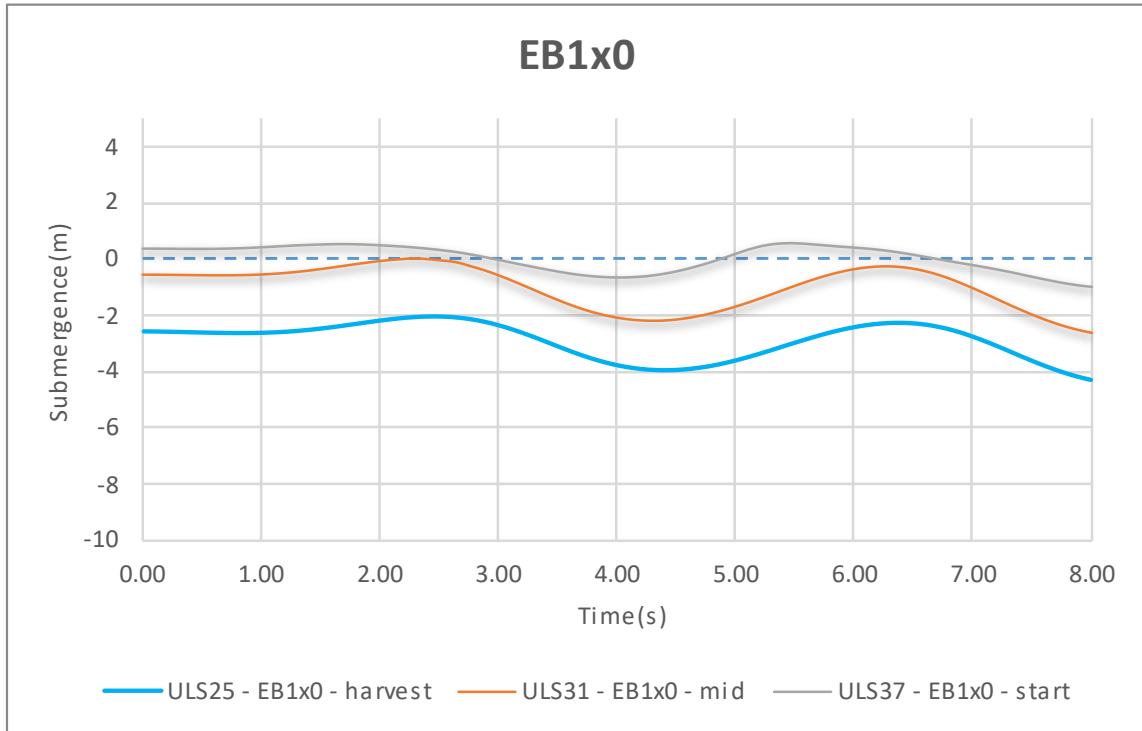


Figure 13 - Buoy Simulation – buoy EB1x0 submersion end buoy – Environment 2

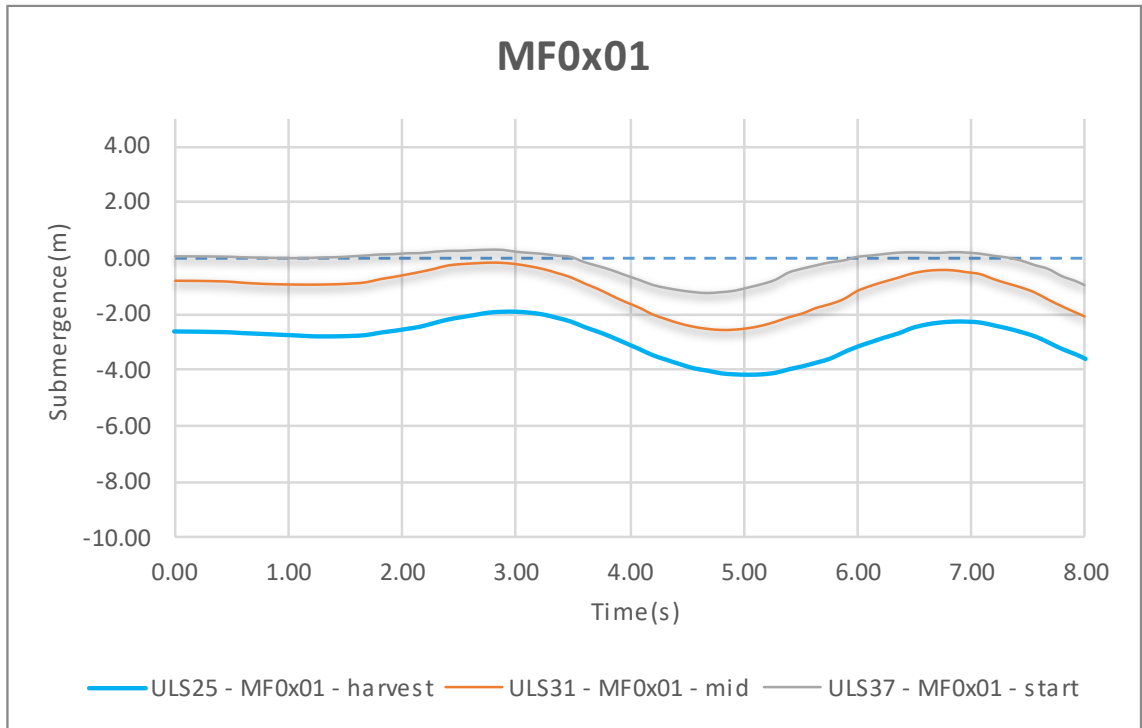


Figure 12 - Buoy Simulation – buoy MF0x01 submersion mussel floats – Environment 2

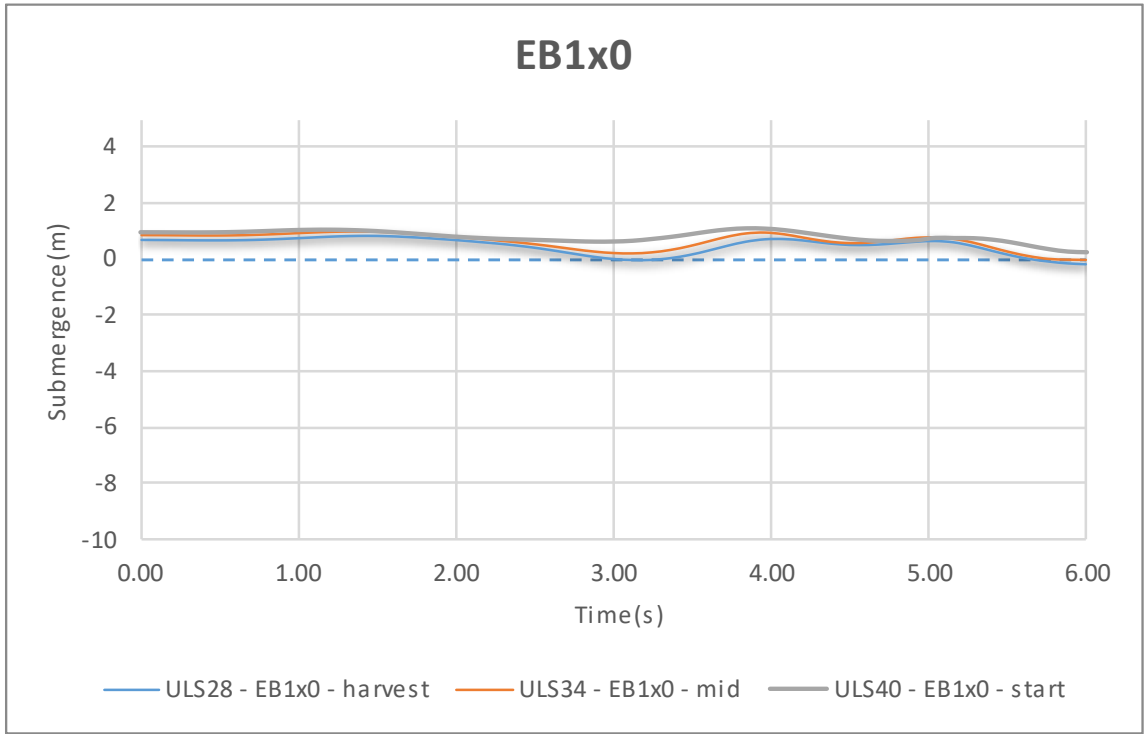


Figure 14 - Buoy Simulation – buoy EB1x0 submersion end buoy – Environment 3

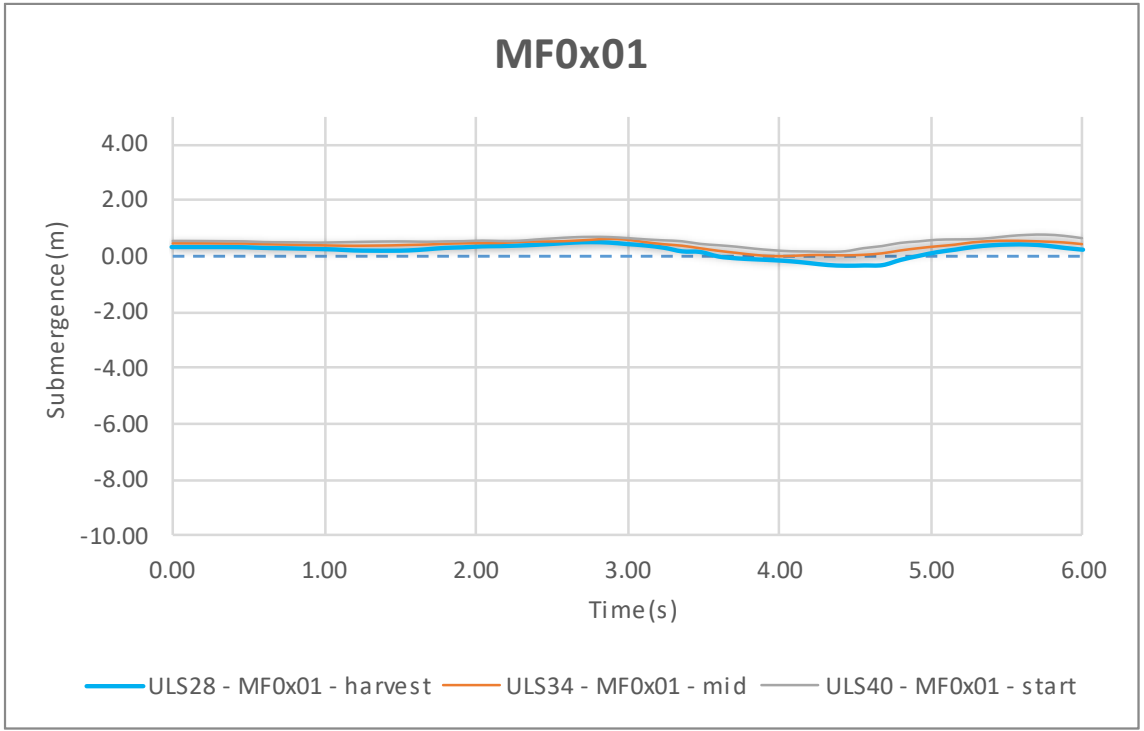


Figure 15 - Buoy Simulation – buoy MF0x01 submersion mussel floats – Environment 3

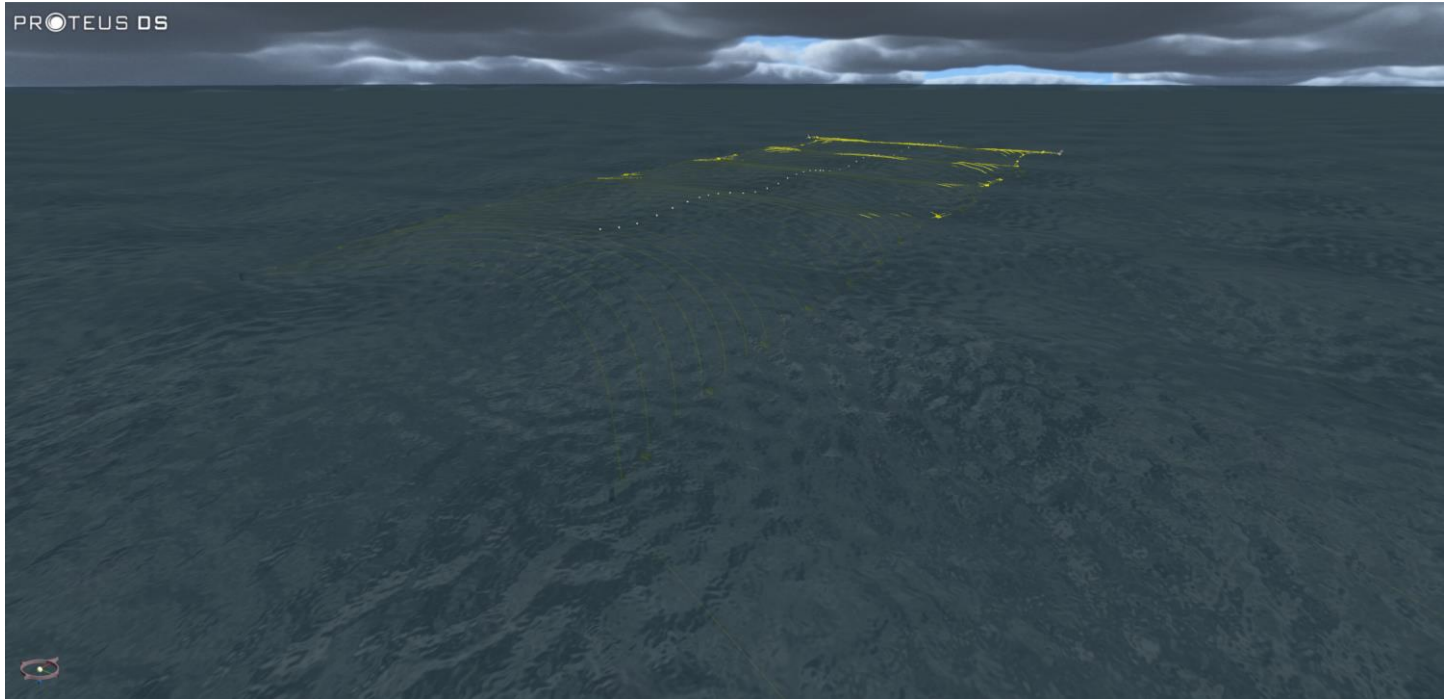


Figure 16 - ULS01 - Rendered View

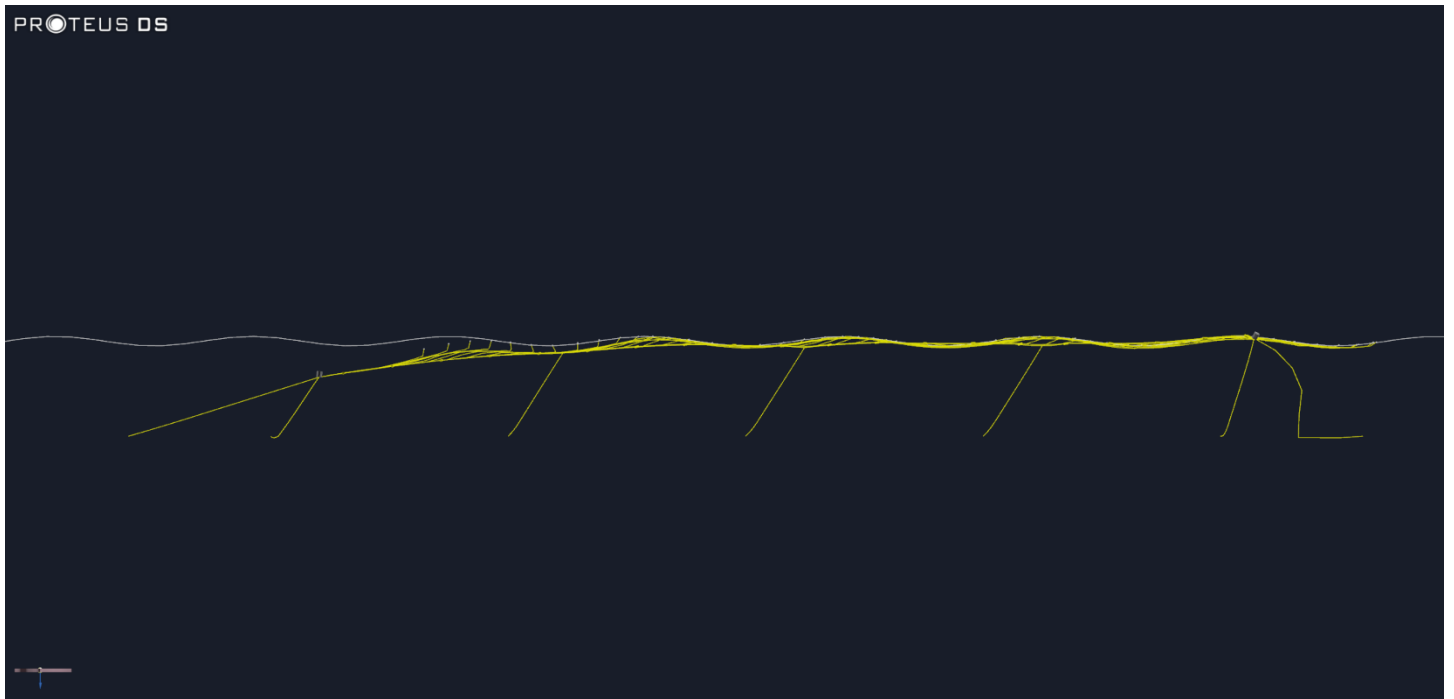


Figure 17 - ULS01 - Elevation

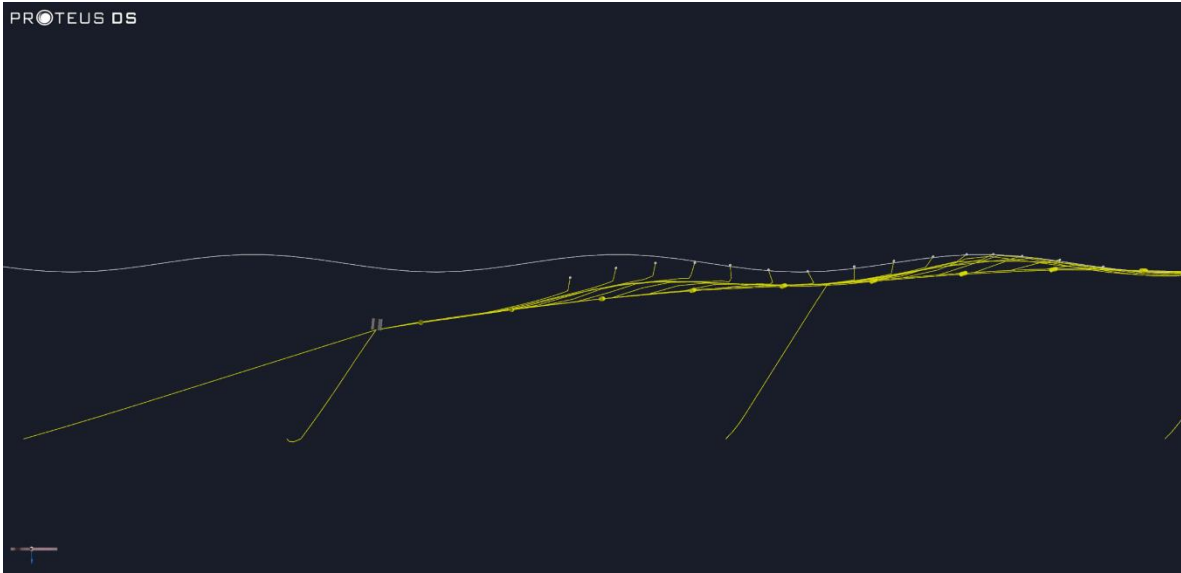


Figure 18 - ULS01 - End Buoy Submergence (harvest) – Environment 1

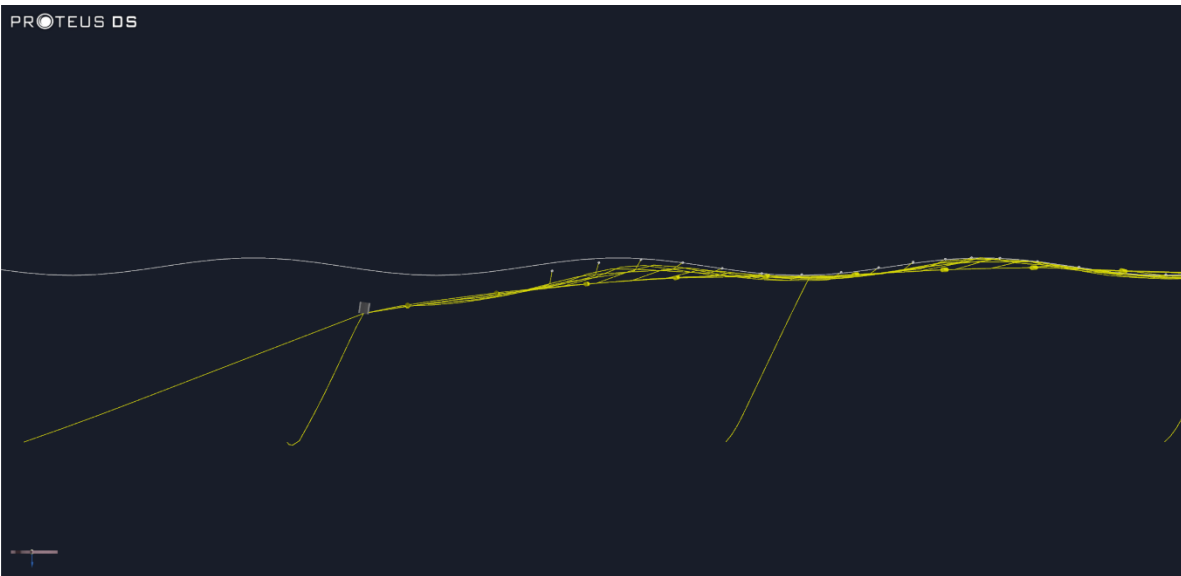


Figure 19 - ULS09 - End Buoy Submergence (mid) – Environment 1

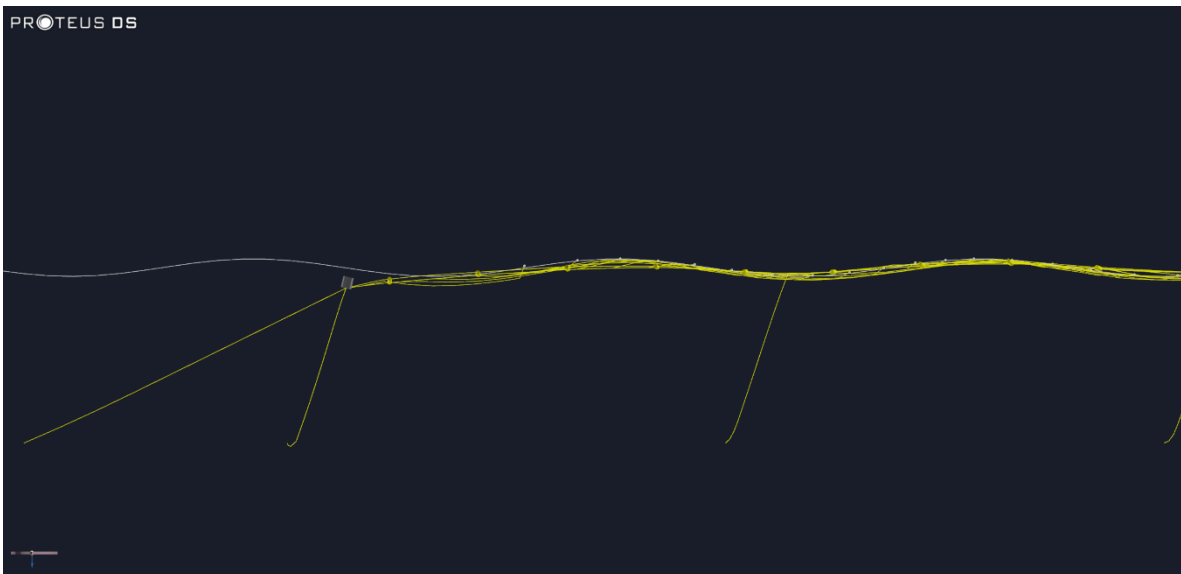


Figure 20 - ULS17 - End Buoy Submergence (start) – Environment 1

5 Minimum Safety Factors – Harvest State Across all Environments

Table 14: Mooring Line Minimum Safety Factors – Harvest state – Environment 1

Values highlighted in red are the minimum Factor of Safety for that component across all scenarios.

| Mooring | Segment | FOS of Studies | | | | | | | | Min FOS ULS |
|-----------|-----------------------|-----------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------|
| | | ULS01_Harvest_0 | ULS02_Harvest_45 | ULS03_Harvest_90 | ULS04_Harvest_135 | ULS05_Harvest_180 | ULS06_Harvest_225 | ULS07_Harvest_270 | ULS08_Harvest_315 | |
| Mooring01 | PolySteel_3_Strand_32 | 1.42 | 2.44 | 40.76 | >100 | >100 | 29.40 | 4.00 | 1.83 | 1.42 |
| Mooring01 | U2_StudLink_32 | 5.19 | 8.94 | >100 | >100 | >100 | >100 | 14.62 | 6.68 | 5.19 |
| Mooring02 | PolySteel_3_Strand_32 | 1.42 | 1.83 | 4.00 | 26.54 | >100 | >100 | 37.71 | 2.47 | 1.42 |
| Mooring02 | U2_StudLink_32 | 5.19 | 6.68 | 14.63 | 97.11 | >100 | >100 | >100 | 9.06 | 5.19 |
| Mooring03 | PolySteel_3_Strand_32 | 41.90 | 7.49 | 4.29 | 5.29 | 19.22 | 79.35 | >100 | >100 | 4.29 |
| Mooring03 | U2_StudLink_32 | >100 | 27.40 | 15.68 | 19.34 | 70.34 | >100 | >100 | >100 | 15.68 |
| Mooring04 | PolySteel_3_Strand_32 | 5.62 | 2.71 | 2.12 | 2.70 | 6.24 | >100 | >100 | >100 | 2.12 |
| Mooring04 | U2_StudLink_32 | 20.57 | 9.93 | 7.74 | 9.89 | 22.85 | >100 | >100 | >100 | 7.74 |
| Mooring05 | PolySteel_3_Strand_32 | 5.70 | 2.71 | 2.15 | 2.71 | 5.70 | >100 | >100 | >100 | 2.15 |
| Mooring05 | U2_StudLink_32 | 20.86 | 9.91 | 7.87 | 9.90 | 20.87 | >100 | >100 | >100 | 7.87 |
| Mooring06 | PolySteel_3_Strand_32 | 6.23 | 2.70 | 2.12 | 2.71 | 5.62 | >100 | >100 | >100 | 2.12 |
| Mooring06 | U2_StudLink_32 | 22.80 | 9.89 | 7.74 | 9.93 | 20.57 | >100 | >100 | >100 | 7.74 |
| Mooring07 | PolySteel_3_Strand_32 | 19.33 | 5.29 | 4.29 | 7.49 | 41.91 | >100 | >100 | >100 | 4.29 |
| Mooring07 | U2_StudLink_32 | 70.75 | 19.35 | 15.69 | 27.40 | >100 | >100 | >100 | >100 | 15.69 |
| Mooring08 | PolySteel_3_Strand_32 | >100 | 32.08 | 4.00 | 1.83 | 1.42 | 2.48 | 34.91 | 98.70 | 1.42 |
| Mooring08 | U2_StudLink_32 | >100 | >100 | 14.63 | 6.68 | 5.19 | 9.06 | >100 | >100 | 5.19 |
| Mooring09 | PolySteel_3_Strand_32 | >100 | >100 | 41.07 | 2.44 | 1.42 | 1.83 | 3.98 | 31.70 | 1.42 |
| Mooring09 | U2_StudLink_32 | >100 | >100 | >100 | 8.94 | 5.19 | 6.68 | 14.58 | >100 | 5.19 |
| Mooring10 | PolySteel_3_Strand_32 | 18.91 | >100 | 80.62 | >100 | 41.84 | 7.50 | 4.26 | 5.26 | 4.26 |
| Mooring10 | U2_StudLink_32 | 69.21 | >100 | >100 | >100 | >100 | 27.44 | 15.59 | 19.26 | 15.59 |
| Mooring11 | PolySteel_3_Strand_32 | 6.24 | >100 | >100 | >100 | 5.62 | 2.72 | 2.10 | 2.70 | 2.10 |
| Mooring11 | U2_StudLink_32 | 22.82 | >100 | >100 | >100 | 20.56 | 9.95 | 7.69 | 9.89 | 7.69 |
| Mooring12 | PolySteel_3_Strand_32 | 5.71 | >100 | >100 | >100 | 5.71 | 2.72 | 2.14 | 2.72 | 2.14 |
| Mooring12 | U2_StudLink_32 | 20.91 | >100 | >100 | >100 | 20.90 | 9.94 | 7.84 | 9.94 | 7.84 |
| Mooring13 | PolySteel_3_Strand_32 | 5.62 | >100 | >100 | >100 | 6.25 | 2.71 | 2.10 | 2.72 | 2.10 |
| Mooring13 | U2_StudLink_32 | 20.57 | >100 | >100 | >100 | 22.88 | 9.90 | 7.70 | 9.95 | 7.70 |
| Mooring14 | PolySteel_3_Strand_32 | 41.78 | >100 | >100 | >100 | 19.11 | 5.28 | 4.26 | 7.50 | 4.26 |
| Mooring14 | U2_StudLink_32 | >100 | >100 | >100 | >100 | 69.91 | 19.31 | 15.58 | 27.44 | 15.58 |

Table 15: Grid Line Minimum Safety Factors – Harvest state – Environment 1

Values highlighted in red are the minimum Factor of Safety for that component across all scenarios.

| Gridline | Segment | FOS of Studies | | | | | | | | Min FOS ULS |
|---------------|-----------------------|-----------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------|
| | | ULS01_Harvest_0 | ULS02_Harvest_45 | ULS03_Harvest_90 | ULS04_Harvest_135 | ULS05_Harvest_180 | ULS06_Harvest_225 | ULS07_Harvest_270 | ULS08_Harvest_315 | |
| GridlineY0x0b | PolySteel_3_Strand_32 | 2.41 | 2.74 | 3.71 | 2.74 | 2.41 | 3.80 | 35.65 | 3.80 | 2.41 |
| GridlineY0x1b | PolySteel_3_Strand_32 | 3.90 | 8.43 | 77.74 | 8.39 | 3.90 | 4.84 | 5.92 | 4.84 | 3.90 |
| GridlineY0x0a | PolySteel_3_Strand_32 | 3.90 | 4.84 | 5.94 | 4.83 | 3.90 | 8.81 | 96.40 | 8.76 | 3.90 |
| GridlineY0x1a | PolySteel_3_Strand_32 | 2.41 | 3.78 | 43.89 | 3.78 | 2.41 | 2.74 | 3.69 | 2.74 | 2.41 |

Table 16: Mooring Line Minimum Safety Factors – Harvest state – Environment 2

Values highlighted in red are the minimum Factor of Safety for that component across all scenarios.

| Mooring | Segment | FOS of Studies | | | Min FOS ULS |
|-----------|-----------------------|------------------|-------------------|-------------------|-------------|
| | | ULS25_Harvest2_0 | ULS26_Harvest2_45 | ULS27_Harvest2_90 | |
| Mooring01 | PolySteel_3_Strand_32 | 2.18 | 3.80 | 46.24 | 2.18 |
| Mooring01 | U2_StudLink_32 | 7.98 | 13.89 | >100 | 7.98 |
| Mooring02 | PolySteel_3_Strand_32 | 2.18 | 2.63 | 4.93 | 2.18 |
| Mooring02 | U2_StudLink_32 | 7.99 | 9.62 | 18.03 | 7.99 |
| Mooring03 | PolySteel_3_Strand_32 | 48.48 | 10.26 | 6.11 | 6.11 |
| Mooring03 | U2_StudLink_32 | >100 | 37.53 | 22.36 | 22.36 |
| Mooring04 | PolySteel_3_Strand_32 | 9.20 | 3.87 | 3.10 | 3.10 |
| Mooring04 | U2_StudLink_32 | 33.65 | 14.18 | 11.35 | 11.35 |
| Mooring05 | PolySteel_3_Strand_32 | 10.31 | 4.05 | 3.16 | 3.16 |
| Mooring05 | U2_StudLink_32 | 37.74 | 14.82 | 11.57 | 11.57 |
| Mooring06 | PolySteel_3_Strand_32 | 11.19 | 4.03 | 3.10 | 3.10 |
| Mooring06 | U2_StudLink_32 | 40.97 | 14.76 | 11.35 | 11.35 |
| Mooring07 | PolySteel_3_Strand_32 | 23.14 | 7.43 | 6.11 | 6.11 |
| Mooring07 | U2_StudLink_32 | 84.68 | 27.18 | 22.35 | 22.35 |
| Mooring08 | PolySteel_3_Strand_32 | >100 | 28.81 | 4.92 | 4.92 |
| Mooring08 | U2_StudLink_32 | >100 | >100 | 18.01 | 18.01 |
| Mooring09 | PolySteel_3_Strand_32 | 87.96 | >100 | 45.25 | 45.25 |
| Mooring09 | U2_StudLink_32 | >100 | >100 | >100 | 165.57 |
| Mooring10 | PolySteel_3_Strand_32 | 23.17 | >100 | >100 | 23.17 |
| Mooring10 | U2_StudLink_32 | 84.77 | >100 | >100 | 84.77 |
| Mooring11 | PolySteel_3_Strand_32 | 11.13 | >100 | >100 | 11.13 |
| Mooring11 | U2_StudLink_32 | 40.74 | >100 | >100 | 40.74 |
| Mooring12 | PolySteel_3_Strand_32 | 10.30 | >100 | >100 | 10.30 |
| Mooring12 | U2_StudLink_32 | 37.68 | >100 | >100 | 37.68 |
| Mooring13 | PolySteel_3_Strand_32 | 9.20 | >100 | >100 | 9.20 |
| Mooring13 | U2_StudLink_32 | 33.66 | >100 | >100 | 33.66 |
| Mooring14 | PolySteel_3_Strand_32 | 48.04 | >100 | >100 | 48.04 |
| Mooring14 | U2_StudLink_32 | >100 | >100 | >100 | 175.82 |

Table 17: Grid Line Minimum Safety Factors – Harvest state – Environment 2

Values highlighted in red are the minimum Factor of Safety for that component across all scenarios.

| Gridline | Segment | FOS of Studies | | | Min FOS ULS |
|---------------|-----------------------|------------------|-------------------|-------------------|-------------|
| | | ULS25_Harvest2_0 | ULS26_Harvest2_45 | ULS27_Harvest2_90 | |
| GridlineY0x0b | PolySteel_3_Strand_32 | 3.73 | 3.95 | 5.38 | 3.73 |
| GridlineY0x1b | PolySteel_3_Strand_32 | 6.76 | 17.27 | 83.16 | 6.76 |
| GridlineY0x0a | PolySteel_3_Strand_32 | 6.76 | 7.52 | 8.52 | 6.76 |
| GridlineY0x1a | PolySteel_3_Strand_32 | 3.73 | 5.23 | 56.60 | 3.73 |

Table 18: Mooring Line Minimum Safety Factors – Harvest state – Environment 3

Values highlighted in red are the minimum Factor of Safety for that component across all scenarios.

| Mooring | Segment | FOS of Studies | | | Min FOS ULS |
|-----------|-----------------------|------------------|-------------------|-------------------|-------------|
| | | ULS28_Harvest3_0 | ULS29_Harvest3_45 | ULS30_Harvest3_90 | |
| Mooring01 | PolySteel_3_Strand_32 | 6.65 | 20.34 | 54.71 | 6.65 |
| Mooring01 | U2_StudLink_32 | 24.34 | 74.42 | >100 | 24.34 |
| Mooring02 | PolySteel_3_Strand_32 | 6.63 | 5.67 | 9.23 | 5.67 |
| Mooring02 | U2_StudLink_32 | 24.28 | 20.73 | 33.76 | 20.73 |
| Mooring03 | PolySteel_3_Strand_32 | 88.18 | 18.14 | 12.85 | 12.85 |
| Mooring03 | U2_StudLink_32 | >100 | 66.38 | 47.01 | 47.01 |
| Mooring04 | PolySteel_3_Strand_32 | 51.67 | 8.44 | 7.08 | 7.08 |
| Mooring04 | U2_StudLink_32 | >100 | 30.90 | 25.89 | 25.89 |
| Mooring05 | PolySteel_3_Strand_32 | 58.02 | 9.53 | 7.26 | 7.26 |
| Mooring05 | U2_StudLink_32 | >100 | 34.87 | 26.56 | 26.56 |
| Mooring06 | PolySteel_3_Strand_32 | 48.73 | 9.68 | 7.09 | 7.09 |
| Mooring06 | U2_StudLink_32 | >100 | 35.41 | 25.96 | 25.96 |
| Mooring07 | PolySteel_3_Strand_32 | 84.44 | 16.30 | 12.84 | 12.84 |
| Mooring07 | U2_StudLink_32 | >100 | 59.64 | 46.99 | 46.99 |
| Mooring08 | PolySteel_3_Strand_32 | >100 | 39.61 | 9.36 | 9.36 |
| Mooring08 | U2_StudLink_32 | >100 | >100 | 34.24 | 34.24 |
| Mooring09 | PolySteel_3_Strand_32 | >100 | >100 | 53.81 | 53.81 |
| Mooring09 | U2_StudLink_32 | >100 | >100 | >100 | 196.90 |
| Mooring10 | PolySteel_3_Strand_32 | 76.47 | >100 | >100 | 76.47 |
| Mooring10 | U2_StudLink_32 | >100 | >100 | >100 | 279.84 |
| Mooring11 | PolySteel_3_Strand_32 | 42.82 | >100 | >100 | 42.82 |
| Mooring11 | U2_StudLink_32 | >100 | >100 | >100 | 156.69 |
| Mooring12 | PolySteel_3_Strand_32 | 47.39 | >100 | >100 | 47.39 |
| Mooring12 | U2_StudLink_32 | >100 | >100 | >100 | 173.40 |
| Mooring13 | PolySteel_3_Strand_32 | 47.03 | 74.75 | >100 | 47.03 |
| Mooring13 | U2_StudLink_32 | >100 | >100 | >100 | 172.10 |
| Mooring14 | PolySteel_3_Strand_32 | 94.88 | 72.90 | >100 | 72.90 |
| Mooring14 | U2_StudLink_32 | >100 | >100 | >100 | 266.79 |

Table 19: Grid Line Minimum Safety Factors – Harvest state – Environment 3

Values highlighted in red are the minimum Factor of Safety for that component across all scenarios.

| Gridline | Segment | FOS of Studies | | | Min FOS ULS |
|---------------|-----------------------|------------------|-------------------|-------------------|-------------|
| | | ULS28_Harvest3_0 | ULS29_Harvest3_45 | ULS30_Harvest3_90 | |
| GridlineY0x0b | PolySteel_3_Strand_32 | 9.94 | 7.37 | 10.80 | 7.37 |
| GridlineY0x1b | PolySteel_3_Strand_32 | 28.18 | 74.17 | >100 | 28.18 |
| GridlineY0x0a | PolySteel_3_Strand_32 | 29.41 | 19.01 | 18.22 | 18.22 |
| GridlineY0x1a | PolySteel_3_Strand_32 | 9.70 | 21.83 | 60.68 | 9.70 |

6 Conclusion

The design has been evaluated in accordance with Scottish Technical Standard for Finfish Aquaculture. The tables below show the highest loaded lines in the harvest state of environment 1 and their factors of safety compared with the requirement of the standard for a given material.

| Line | Segment | Max Tension ULS (T) | Min FOS ULS | Found in | ULS Material Factor |
|---------------|-----------------------|---------------------|-------------|----------|---------------------|
| Mooring02 | PolySteel_3_Strand_32 | 11.44 | 1.42 | ULS01 | 3.00 |
| | U2_StudLink_32 | 11.44 | 5.19 | ULS01 | 2.00 |
| GridlineY0x0a | PolySteel_3_Strand_32 | 4.17 | 3.90 | ULS01 | 3.00 |
| GridlineY0x0b | PolySteel_3_Strand_32 | 6.75 | 2.41 | ULS01 | 3.00 |

Definitions

| | |
|-------------------------------|--|
| 10-year data | A statistical evaluation of the probable conditions which will occur at the given location in a ten-year period. 10-year data is linked to and will always have lower values than 50-year data. |
| 50-year data | A statistical evaluation of the probable conditions which will occur at the given location in a fifty-year period. 50-year data is linked to and will always have higher values than 10-year data. |
| Dynamic Analysis | Evaluation of the system taking account of the change of loads over time through such characteristics as wave loading. |
| Element | The smallest section of a line which is utilised for the evaluation of loads on that line. |
| Finite Element Analysis (FEA) | The process of breaking down all lines into small discrete elements allowing the calculation of loads and stresses to be undertaken on a complex system. The loads calculated at the end of the element are used as the input loads to the adjoining element, therefor allowing repetition of the process through the complete system. |
| H_{max} | Maximum wave height (trough to crest) within the spectrum which makes up the significant wave height, for the purpose of modelling this is calculated as $1.9 \times H_s$ |
| H_s | Significant wave height, the mean wave height (trough to crest) of the highest third of the waves. |
| Line | A rope, chain, strop or combination thereof which connects nodes within the mooring system, such as a mooring line, which connects an anchor to a connection on the grid. |
| Minimum Break Load (MBL) | The minimum guaranteed load which a component will carry before failure. |
| Safety Factor | The MBL of a component divided by the highest load applying upon it. |
| Segment | The section of a line made up by a single material, for example a mooring line may be made up of both chain and rope, it will therefore have two segments, one segment will be the length of the chain, the other segment will be the length of the rope. |
| Submersion | Distance below the surface of the water. |

| | |
|----------------------|---|
| T_p | Wave period |
| Ultimate Limit State | Evaluation of the system in its normal, fully intact operating state. |
| γ_l | Load Factor, a safety factor applied to components to take account of the uncertainty or error involved in calculating loads. Specified within the applicable Standard. |
| γ_m | Material Factor, a safety factor applied to components to take account of the variation in materials when manufacturing components. Specified within the applicable Standard. |

References

- (1) Marine Scotland: A Technical Standard for Scottish Finfish Aquaculture
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